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## A NOTE ON THE THEORY AND PRACTISE OF MULTIPLICATIVE RATE MAKING

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0. Introduction

A tariff is a rule for the division of an insurance portfolio into disjoint classes or cells, and an assignment of a premium  $f_c$  to each cell  $c$ .

The premiums  $f_c$  constitute a vector, the dimension of which is equal to the number of cells. A tariff structure or a tariff model is described by specifying a surface in this vector space, on which the premium point with coordinates  $f_c$  is required to be situated. The dimensionality of this surface is called the number of free parameters or the number of degrees of freedom of the model.

The simplest structure is the one which assigns the same premium to all cells. Its surface consists of the straight line of points with all coordinates equal. The number of degrees of freedom is obviously equal to one, the free parameter being the common premium.

In the following we will assume that a basic subdivision has already been done.

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# 1. The likelihood function of tariff construction

In general, when we want to construct or modify a tariff the statistical material at hand will (or should) consist of, for each cell  $c$ ,

- exposure  $n_c$  (e.g. number of policy years, or amount insured times years at risk, or premiums)
- claims frequency  $s_c$  (number of claims per unit of exposure)
- observed risk premiums  $p_c$  (claims amount per unit of exposure)

We denote by

- $\lambda_c$  the theoretical claims frequency for cell  $c$
- $\mu_c$  the expected value of the size of an individual claim in cell  $c$  (theoretical average claims size)
- $\pi_c$  the theoretical risk premium in cell  $c$ ,  $\pi_c = \lambda_c \mu_c$ .

We assume numbers of claims to be Poisson distributed. The probability of  $k$  claims in cell  $c$  is then

$$(n_c \lambda_c)^k \exp(-n_c \lambda_c) / k!$$

We denote by

- $\sigma_c$  the standard deviation of the individual claims sizes in cell  $c$

and we assume that, given  $k$  claims, the total claims amount in cell  $c$  has a Normal distribution with mean  $k\mu_c$  and s.d.  $\sigma_c \sqrt{k}$

The likelihood function  $L$  corresponding to the observed frequencies  $s_c$  and risk premiums  $p_c$  (i.e. the a priori probability of the statistical material) will then be as follows, assuming the cells to be stochastically independent. The observed  $k$ -value in cell  $c$  is  $n_c s_c$ , and the observed total claims amount is  $n_c p_c$ .

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$$(1) \quad \begin{cases} L(\lambda_c, \mu_c, \sigma_c) = L_1(\lambda_c) \cdot L_2(\mu_c, \sigma_c) \\ L_1(\lambda_c) = \frac{\pi(n_c \lambda_c)}{c^{n_c \lambda_c}} \exp(-n_c \lambda_c) / (n_c s_c)! \\ L_2(\mu_c, \sigma_c) = \frac{\pi(2\pi n_c s_c)^{1/2} \sigma_c^{-1}}{c} \exp\{-(n_c p_c - n_c s_c \mu_c)^2 / 2 n_c s_c \sigma_c^2\} \end{cases}$$

The function  $L$  should be maximized w.r.to the parameters  $\lambda_c, \mu_c, \sigma_c$ . This should be done under the constraints imposed on the parameters by the tariff model chosen.

## 2. Likelihood theory for multiplicative rate making

In multiplicative rate making one specifies for  $\pi_c = \lambda_c \mu_c$  a multiplicative expression with one factor for each premium argument which is taken into consideration. For simplicity of notation, we assume the number of premium arguments to be three. The premium arguments may take on  $m_1, m_2$  and  $m_3$  different values, respectively.

The number of cells is then  $m = m_1 m_2 m_3$  and the general cell index  $c$  is replaced by  $ijk$  ( $i = 1 \dots m_1, j = 1 \dots m_2, k = 1 \dots m_3$ )

Risk premiums  $\pi_c$  are required to be of the form  $\pi_{ijk} = \bar{p} u_i v_j w_k$ , i.e. the likelihood function

$$(2) \quad L(\lambda_{ijk}, \mu_{ijk}, \sigma_{ijk}) = L_1(\lambda_{ijk}) \cdot L_2(\mu_{ijk}, \sigma_{ijk})$$

should be maximized under the constraints

$$(3) \quad \lambda_{ijk} \mu_{ijk} = \bar{p} u_i v_j w_k$$

Here,  $\bar{p}$  is the observed overall riskpremium, while  $u_i, v_j, w_k$  are nonnegative parameters. These are free parameters apart from a proportionality normalization. The latter can e.g. be of the form  $u_1 = v_1 = w_1$  from which it is seen that there are  $1 + (m_1 - 1) + (m_2 - 1) + (m_3 - 1) = d$  free parameters of this kind.

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In addition we have the  $\lambda_{ijk}$  as free parameters. When they are also determined we get the  $\mu_{ijk}$  from

$$(4) \quad \mu_{ijk} = \bar{p} u_i v_j w_k / \lambda_{ijk}$$

We now have  $(d+m)$  free parameters. Finally, the standard deviations  $\sigma_{ijk}$  are also assumed to be unknown. To be able to estimate them from the observed data we have to make simplifying assumptions, e.g.

$$(5) \quad \sigma_{ijk} \text{ all equal, say } \sigma_{ijk} = \sigma$$

or

$$(6) \quad \sigma_{ijk} \text{ proportional to } \mu_{ijk}, \sigma_{ijk} = \sigma \mu_{ijk}$$

or, as an intermediate case,

$$(7) \quad \sigma_{ijk} \text{ proportional to } \sqrt{\mu_{ijk}}, \sigma_{ijk} = \sigma \sqrt{\mu_{ijk}}$$

In all three cases, the total number of free parameters, i.e. the number of degrees of freedom, will be  $d+m+1$ .

In order to estimate the parameters we should maximize (2) taking into consideration the constraint (4) and one of the alternative constraints (5), (6) and (7).

We adopt the following approximate procedure. In (2) the first factor  $L_1(\lambda_{ijk})$  is maximized by putting theoretical frequencies equal to the observed ones, i.e.

$$\hat{\lambda}_{ijk} = s_{ijk}$$

Then there remains the maximization of

$$L_2(\mu_{ijk}, \sigma_{ijk}). \text{ From (4)}$$

$$(8) \quad \mu_{ijk} = \bar{p} u_i v_j w_k / s_{ijk}$$

and from (1)

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$$(9) \quad L_2(u_{ijk}, \sigma_{ijk}) = \text{const} \cdot \prod_{ijk} \sigma_{ijk}^{-1} \cdot \exp(-Q/2)$$

with

$$(10) \quad Q = \sum_{ijk} n_{ijk} (p_{ijk} - \bar{p} u_i v_j w_k)^2 / s_{ijk} \sigma_{ijk}^2$$

Under the constraint (5),  $\sigma_{ijk} = \sigma$ , the maximization of  $L_2$  is equivalent to minimizing, with respect to  $u_i, v_j, w_k$

$$Q_a = \sum_{ijk} n_{ijk} (p_{ijk} - \bar{p} u_i v_j w_k)^2 / s_{ijk}$$

i.e. Least squares with  $n_{ijk}/s_{ijk}$  as weights.

Then  $\hat{\sigma}$  is obtained by

$$\hat{\sigma}^2 = \hat{Q}_a / m$$

Of the two constraints (6) and (7) we choose to treat (7) in some more detail. Under this constraint, (8)-(10) yield

$$(11) \quad L_2(u_i, v_j, w_k, \sigma) = \text{Const} \cdot \sigma^{-m} \cdot \prod_{ijk} (u_i v_j w_k)^{-1/2} \cdot \exp(-Q/2)$$

with

$$Q = \sigma^{-2} \sum_{ijk} n_{ijk} (p_{ijk} - \bar{p} u_i v_j w_k)^2 / \bar{p} u_i v_j w_k = \sigma^{-2} Q_A$$

To maximize  $L_2$  or, equivalently,  $\log L_2$  we put the partial derivatives of  $\log L_2$  w.r. to  $\sigma, u_i (i=1 \dots m_1), v_j (j=1 \dots m_2), w_k (k=1 \dots m_3)$  equal to zero. Observing that

$$(12) \quad Q_A = \left[ \sum_{ijk} n_{ijk} \frac{p_{ijk}^2}{\bar{p} u_i v_j w_k} - 2 \sum_{ijk} n_{ijk} p_{ijk} + \sum_{ijk} n_{ijk} \bar{p} u_i v_j w_k \right]$$





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To solve the system (13), we may choose an initial value for  $\sigma$  and then solve equations (13b) for  $u_i, v_j, w_k$  (it can be proved that there is one, essentially unique, solution). Putting the values obtained for  $u_i, v_j, w_k$  into (13a), we get a new value for  $\sigma$  and repeat the procedure. The process is stopped when two successive  $\sigma$ -values are equal.

From (11) and (13a) we then have

$$(14) \quad \hat{Q} = \hat{\sigma}^{-2} \hat{Q}_A = m = \text{Const}$$

and

$$(15) \quad 2\text{Log}\hat{L}_2 = \text{Const} - m\text{Log}\hat{Q}_A - m_2 m_3 \sum_i \text{Log}\hat{u}_i - m_1 m_3 \sum_j \text{Log}\hat{v}_j - \\ - m_1 m_2 \sum_k \text{Log}\hat{w}_k$$

As earlier pointed out, the number of degrees of freedom is  $(m_1 + m_2 + m_3 - 2) + m + 1$ . The three terms in this sum correspond, respectively, to the factors  $u, v$  and  $w$ , to the estimated frequencies and to  $\sigma$ .

If we want to test e.g. the hypothesis that all  $w_k$  can be put equal to one, i.e. the third factor variable has no influence, we have to solve the system (13) putting all  $w_k = 1$  (the third line of (13b) should be omitted, of course). If the estimates obtained are denoted by two "hats", the likelihood test statistic becomes

$$2\text{Log}\hat{L}_2 - 2\text{Log}\hat{\hat{L}}_2 = (-m\text{Log}\hat{Q}_A - m_2 m_3 \sum_i \text{Log}\hat{u}_i - m_1 m_3 \sum_j \text{Log}\hat{v}_j - \\ - m_1 m_2 \sum_k \text{Log}\hat{w}_k) - (-m\text{Log}\hat{\hat{Q}}_A - m_2 m_3 \sum_i \text{Log}\hat{\hat{u}}_i - m_1 m_3 \sum_j \text{Log}\hat{\hat{v}}_j)$$

It is approximatively chi-square distributed with degrees of freedom equal to

$$(m_1 m_2 + m_3 - 2) - (m_1 + m_2 - 1) = m_3 - 1$$

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For comparisons of one factor model with a more specialized one, the important part of  $2\text{Log}L_2$  is, therefore, minus  $m$  times the sum of

$$\text{Log}Q_A$$

and, for each factor variable,

the arithmetic mean of the logarithms of the factors

The relevant part of the number of degrees of freedom equals the total number of factors minus the number of factor variables plus one.

### 3. An example of multiplicative rate making practise

In practical work the theory above has been used in the following simplified, and somewhat rough, way.

To solve the system (13), we put the initial value for  $\sigma$  equal to zero. Equations (13b) are then solved with their right-hand members equal to zero. This means putting the partial derivatives of  $Q_A$  w.r. to  $u_i, v_j, w_k$  equal to zero. The estimates obtained are thus those which minimize  $Q_A$ .

We then compute  $\sigma^2$  from (13a) and assume that if this  $\sigma^2$  was inserted in (13b), and (13b) was solved for  $u_i, v_j, w_k$ , we would get roughly the same  $\sigma^2$  back from (13a). In reality, we would, of course, obtain a larger  $\sigma^2$  as  $Q_A$  would increase somewhat from its minimum value.

Thus we assume that the iteration would (approximately) stop after one further step, and so we do not have to carry it through to obtain  $\sigma^2$ :

$$m\hat{\sigma}^2 = \hat{Q}_A = \text{minimum } Q_A \text{ w.r. to } u, v, w.$$

From (12) and (13b) with right hand members equal to zero, we get

$$\min Q_A = \hat{Q}_A = 2 \sum_{ijk} \bar{p}_{ijk} u_i v_j w_k - 2 \sum_{ijk} p_{ijk}$$

i.e.

$$\hat{Q}_A = 2 (\text{graduated} - \text{observed claims cost})$$

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where the graduation is done by those factors  $u, v, w$  which minimize  $Q_A$ . This coincides with the original Boehm-Mehring program [ ] for fitting a multiplicative model.

As  $\hat{Q}_A$  is positive, the factors  $u, v$  and  $w$  thus far obtained overestimate the observed claims cost. Instead of carrying through the iterations to the end, we now adopt Jung's [ ] approach to estimate the factors. This means that we put not only the total graduated claims cost equal to the observed one, but do so also for each marginal sum.

$$(14) \quad \begin{cases} \sum_{jk} n_{ijk} p_{ijk} - \sum_{jk} n_{ijk} \bar{p}_{i,j,k} u_i v_j w_k = 0 \quad (i = 1 \dots m_1) \\ \sum_{ik} n_{ijk} p_{ijk} - \sum_{ik} n_{ijk} \bar{p}_{i,j,k} u_i v_j w_k = 0 \quad (j = 1 \dots m_2) \\ \sum_{ik} n_{ijk} p_{ijk} - \sum_{ij} n_{ijk} \bar{p}_{i,j,k} u_i v_j w_k = 0 \quad (k = 1 \dots m_3) \end{cases}$$

These equations have one, essentially unique, solution [ ].

This gives us our estimates  $\hat{u}, \hat{v}$  and  $\hat{w}$ .

The quantities  $\hat{Q}_A, \hat{u}, \hat{v}$  and  $\hat{w}$  thus obtained are then used e.g. to construct likelihood ratio tests according to the previous section.

#### 4. The hypothesis of no risk premium differentiation

The simplest tariff model is to assign the same premium to all cells. This may be considered as a multiplicative model with all factors equal,

$$\pi_{ijk} = \bar{p} u \quad \text{for all } i, j, k$$

where  $u$  is the only factor to be estimated. The exact likelihood estimate according to section 2 will make graduated and observed claims costs equal, and so

$$\begin{aligned} \hat{u} &= 1 \\ \hat{\sigma}^2 &= \hat{Q}_A = \sum n_{ijk} (p_{ijk} - \bar{p})^2 / \bar{p} \end{aligned}$$



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The important part of  $\text{Log } L_2$  is  $-\text{mLog} \hat{Q}_A$  and the corresponding number of degrees of freedom is equal to one.

If we use, instead, the practical approach of section 3,  $\hat{Q}_A$  is obtained as the minimum of

$$Q_A = \sum n_{ijk} (p_{ijk} - \bar{p}u)^2 / \bar{p}u$$

w.r.to  $u$ . This yields

$$\bar{p}u = (\sum n_{ijk} p_{ijk}^2 / \sum n_{ijk})^{1/2} > \bar{p}$$

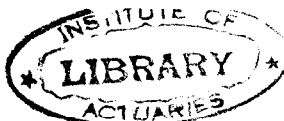
and

$$\hat{Q}_A = 2 \sum n_{ijk} (\bar{p}u - \bar{p})$$

As estimate of the unknown factor  $u$  we still use  $\hat{u} = 1$ .

The simple hypothesis of no premium differentiation between cells can then be tested against a more complicated model by taking the difference between the (important part of)

$\text{Log } L_2$  for the latter and the  $-\text{mLog} \hat{Q}_A$  of this section. Also, one minus the quotient between the two  $\hat{Q}_A$ 's may be taken as a descriptive measure of the variance reduction that is accomplished by the more complicated model.



Description of the multiplicative ratemaking model.

(Free translation from a description by G Andreasson, Oct 1968, augmented by B Ajne and G Green, Dec 1972)

1. The model

Assume that, within a certain branch of insurance, we have tariff arguments  $U, V, W, \dots$ . In motor they could be e.g. make of car, age of car, geographical district etc. In fire we could have e.g. building material (stone, wood,...), year of erection, geographical location etc.

We also have statistical experience consisting of

(1) exposures  $p_{ijk} \dots$

e.g. number of policy years or total sum insured for risks in "cell"  $i, j, k, \dots$

(2) (relative) risk measures  $p_{ijk} \dots$

e.g. claims' cost per policy year or as a proportion of sum insured.

The model assumption is now

$$P_{ijk} \dots = \bar{p} u_i v_j w_k \dots, \text{ where } p \text{ is defined by (3) on p.2}$$

i.e. the influence of the tariff arguments  $U, V, W, \dots$  is assumed to be multiplicative. If the tariff arguments  $U, V, W, \dots$  have  $I, J, K, \dots$  levels, this means that we have replaced the estimation of the  $I \cdot J \cdot K \cdot \dots$  cell risk premiums by the estimation of  $I + J + K + \dots$  risk factors  $u_1 \dots u_I, v_1 \dots v_J, w_1 \dots w_K, \dots$

(  $I, J, K$  are denoted by  $m_1, m_2$  and  $m_3$  in the main paper )

Thus the model assumption implies a considerable reduction of the number of parameters to be estimated from the data. It also supplies a convenient logic for the construction of tariffs, perhaps to a larger extent than an additive model would do as in insurance one is used to express differences in percentages rather than in absolute amounts. Finally, one also gets a possibility to study, via the risk factors, the influence of one tariff argument isolated from those of the others.

## 2. Fitting the model to the data.

Assume for simplicity that we have three tariff arguments  $U, V, W$ . Denote by  $\bar{p}$  the overall risk measure defined by

$$(3) \quad \bar{p} = \frac{\sum_{i,j,k} n_{ijk} p_{ijk}}{\sum_{i,j,k} n_{ijk}}$$

Introduce the normalized risk measures  $r_{ijk}$  defined by

$$(4) \quad r_{ijk} = p_{ijk} / \bar{p}$$

Thus

$$(5) \quad \bar{r} = \sum n_{ijk} r_{ijk} / \sum n_{ijk} = 1$$

The computation starts out from the normalized risk measures, i.e. we start with the estimation problem

$$(6) \quad r_{ijk} \approx u_i v_j w_k$$

Two ways have been used to estimate the  $u$ 's,  $v$ 's and  $w$ 's from the  $r$ 's. The first is the chi square minimum method according to which the following expression should be minimized w.r.to  $u_i, v_j, w_k$ :

$$(7) \quad \chi^2 = \text{cons} \cdot \sum_{i,j,k} n_{ijk} \frac{(u_i v_j w_k - r_{ijk})^2}{u_i v_j w_k}$$

( (7) corresponds to  $Q_A$  in the main paper )

Equating the partial derivatives to zero yields a system of  $I + J + K$  equations for the  $I + J + K$  unknown quantities  $u_i, v_j, w_k$ :

$$\begin{aligned}
 u_i &= \sqrt{\frac{\sum_{j,k} n_{ijk} r_{ijk}^2 / \sum_{j,k} n_{ijk} v_j w_k}{v_j w_k}} \\
 (8) \quad v_j &= \sqrt{\frac{\sum_{i,k} n_{ijk} r_{ijk}^2 / \sum_{i,k} n_{ijk} u_i w_k}{u_i w_k}} \\
 w_k &= \sqrt{\frac{\sum_{i,j} n_{ijk} r_{ijk}^2 / \sum_{i,j} n_{ijk} u_i v_j}{u_i v_j}}
 \end{aligned}$$

( This is system (13b) of the main paper with  $\sigma = 0$  )

The second way could be called the method of unbiased estimation of marginal riskmeasures, which means putting the graduated marginal risk measures equal to the observed ones:

$$(7') \quad \sum_{j,k} n_{ijk} \bar{p}_{i,j,k} = \sum_{j,k} n_{ijk} p_{ijk} \quad (\text{Eq. (14) of main paper})$$

for  $i = 1 \dots I$ , and corresponding equations for each fixed  $j$  and each fixed  $k$ . These equations can be put into the following form, which differs from (8) in that the quantities  $r_{ijk}^2$  have been replaced throughout by  $r_{ijk} u_i v_j w_k$ :

$$\begin{aligned}
 (8') \quad u_i &= \sum_{j,k} n_{ijk} r_{ijk} / \sum_{j,k} n_{ijk} v_j w_k \\
 v_j &= \sum_{i,k} n_{ijk} r_{ijk} / \sum_{i,k} n_{ijk} u_i w_k \\
 w_k &= \sum_{i,j} n_{ijk} r_{ijk} / \sum_{i,j} n_{ijk} u_i v_j
 \end{aligned}$$

Both (8) and (8') are well apt to solution by iteration. Initial values may conveniently be chosen to be the observed marginal risk measures, viz.

$$(9) \quad u_i = \sum_{j,k} n_{ijk} r_{ijk} / \sum n_{ijk}$$

$$v_j = \sum_{i,k} n_{ijk} r_{ijk} / \sum n_{ijk}$$

$$w_k = \sum_{i,j} n_{ijk} r_{ijk} / \sum n_{ijk}$$

According to experience the iteration process converges rapidly, ten steps usually being quite sufficient. In principle the iteration is stopped when the  $m$ :th and  $(m+1)$ :th iteration yields the same result to a certain number of significant figures,

$$(10) \quad {}^{m+1}u_i = {}^m u_i = u_i^*$$

$${}^{m+1}v_j = {}^m v_j = v_j^*$$

$${}^{m+1}w_k = {}^m w_k = w_k^*$$

Hence we get the estimates

$$(11) \quad r_{ijk}^* = u_i^* v_j^* w_k^*$$

and finally

$$(12) \quad p_{ijk}^* = \bar{p} r_{ijk}^*$$

### 3. Testing the goodness of fit.

If the graduation is done according to formulas (7)-(8), chi square minimum, the fit of the model to the data can be tested by computing the quantity  $S$  defined by

$$(13) \quad S = \frac{\sum n_{ijk} u_i^* v_j^* w_k^*}{\sum n_{ijk} r_{ijk}} \quad \text{According to main paper, section 3,}$$

$$\min \chi^2 = 2 \text{ obs claims} \times (S-1)$$

i.e. graduated total claims cost divided by observed total claims cost. From (7) it can be proved that  $S$  is always greater than one, and the deviation  $(S-1)$  can be used as a measure of the "badness" of fit ( $S=1$  means perfect fit).

Also the following marginal quotients are computed

$$(14) \quad S_{i..} = \sum_{j,k} n_{ijk} u_i v_j w_k / \sum_{j,k} n_{ijk} r_{ijk} \quad i = 1, 2, \dots, v_i$$

$$S_{.j.} = \sum_{i,k} n_{ijk} u_i v_j w_k / \sum_{i,k} n_{ijk} r_{ijk} \quad j = 1, 2, \dots, v_j$$

$$S_{..k} = \sum_{i,j} n_{ijk} u_i v_j w_k / \sum_{i,j} n_{ijk} r_{ijk} \quad k = 1, 2, \dots, v_k$$

and their deviations from one may be used to judge the balance of the graduation.

For the method of graduation described by formulas (7')-(8') all S-values will naturally be equal to one, but for rounding off errors. However, they are still computed as a check.

#### 4. Experience with the multiplicative model.

The multiplicative rate making model has, from the late sixties and onwards, found a fairly extensive use in the graduation of swedish claims' statistics within Motor Insurance.

It is also used, at least in one swedish company, to revise tariffs within Home-owner's Comprehensive, House-owner's Comprehensive, Combined Shop Insurance, Pleasure Boat Insurance etc.

The swedish fire tariff has a multiplicative structure and, thus, is well suited for multiplicative graduation. However, some care has to be taken as to the large fire claims, the influence of which has to be smoothed before the graduation.

Often the graduation according to (7)-(8) is used to test the model, while if the fit is considered satisfactory, formulas (7')-(8') are used to actually estimate the risk factors. The latter method pays a little more attention to the smaller risk groups and also fulfills the condition of equity for the tariff arguments taken one at a time.

Also, in practical tariff work the estimated risk factors are often rounded off to get a nice-looking tariff, or are smoothed by a straight line or otherwise in order to avoid too great discontinuities between closely related riskgroups.

If there are conditions a priori on the structure of the tariff these should if possible be introduced as side conditions in the computations leading to the estimated risk factors. In especial if a priori conditions are so restrictive as to leave free only the influence of one tariff argument, multiplicative graduation is no longer necessary.

# ITERATIVE SOLUTION OF EQ.(8) OF THE "DESCRIPTION" (APP1)

Appendix 2A

A = 1.000      G = 0.0      C = 0.0      D = 0.0      E = 0.0      F = 1.000

N = 8966800.      P = 2.896642      Q = 2.896642      R = 1.000061  
 (Total exposure,  $\Sigma_{nijk}$       ( $\bar{P}$  expected as %) )  
 (Sum insured in WEEK)

STUFF 0      S = 1.089530

0.24777	0.31909	0.96677	0.26837	0.12945	0.91049	2.88682	2.06416	0.51300	0.18590
0.91603	4.69370	0.31014	0.15614	0.89537	0.36547	3.19380	1.39424	0.87958	5.87692
3.87528	1.43274	4.51325	3.73742	2.54897	0.52864	0.46248	0.54022	0.52573	0.70464
0.70457	0.14911	0.46988	0.59776	3.51533					
1.72313	0.97252	0.58015							
2.08495	1.26193	2.93292	1.91525	1.01186	0.58407	0.52834	0.34897	0.37784	0.25422

STUFF 1      S = 1.332819

0.23374	0.29427	1.15750	0.44045	0.48768	1.33834	3.60193	3.09827	0.38589	0.18284
0.74361	3.93192	0.55831	0.50300	1.15923	0.58614	3.59212	2.76643	1.63764	3.37875
4.80874	2.06454	5.02996	5.36216	2.24989	1.36288	0.72400	1.00730	0.78241	1.20848
0.97154	0.20310	0.58081	1.36692	3.08728					
1.76578	0.91664	0.69334							
1.69709	1.18710	3.05781	2.69275	0.93707	0.60855	0.67872	0.56841	0.49736	0.44078



STIFF 10

S = 1.331231

U	0.24757	0.31540	1.15144	0.42460	0.40300	1.41398	3.71393	3.09015	0.39984	0.20605
	0.82918	4.02180	0.52927	0.44648	1.22819	0.56814	3.82730	2.70260	1.47793	3.33218
	5.00977	2.03639	5.09457	5.28410	2.34680	1.22511	0.70272	0.92573	0.77262	1.21403
	0.99327	0.21844	0.61425	1.11243	2.75229					
V	1.82199	0.90928	0.68084							
W	1.68097	1.16664	3.06471	2.74110	0.93731	0.60786	0.69684	0.57696	0.50430	0.45321

I	J	K	L	M	FAKTOR F	LOG F	S-WERTE	N-WERTE	P-WERTF	S*P-WERTF
02					0.24757	-1.396058	1.420887	204259.	0.71752	1.01951
04					0.31540	-1.153919	1.699754	107557.	0.92421	1.57092
11					1.15144	0.141017	1.276405	1481350.	2.80019	3.57417
12					0.42460	-0.856613	1.435064	429943.	0.77731	1.11549
14					0.40300	-0.908827	3.749654	315714.	0.37494	1.40590
15					1.41398	0.346407	1.333318	842067.	2.63715	3.51616
16					3.71393	1.312090	1.425457	141758.	8.36144	11.91888
18					3.09015	1.128221	1.277611	324732.	5.97867	7.63841
21					0.39984	-0.916702	1.309945	42552.	1.48587	1.94641
22					0.20605	-1.579621	1.579278	29681.	0.53846	0.85038
23					0.82918	-0.187321	1.400345	20759.	2.65321	3.71541
24					4.02190	1.391729	1.248915	40951.	13.59493	16.97891
26					0.52927	-0.636249	1.559153	46679.	0.89830	1.40059
27					0.44648	-0.806360	2.153018	579006.	0.45224	0.97364
28					1.22819	0.205540	1.357776	479516.	2.59336	3.52120
31					0.56814	-0.565392	1.419295	262705.	1.05854	1.50238
33					3.82730	1.342158	1.601200	114557.	9.25059	14.81204
34					2.70268	0.994245	1.819105	100276.	4.03831	7.34612
36					1.47793	0.390641	2.334092	50980.	2.54764	5.94643
38					3.33218	1.203627	1.100823	78076.	17.02205	18.73827
42					5.00973	1.611382	1.203177	82478.	11.22446	13.50501
45					2.03639	0.711178	1.183638	481095.	4.14983	4.91189
46					5.09457	1.628174	1.212720	83965.	13.07227	15.85301
48					5.28410	1.664702	1.324579	138700.	10.82514	14.33876
51					2.34690	0.853052	1.429221	68853.	7.38290	10.55179
52					1.22511	0.203031	2.371166	72621.	1.53115	3.63062
53					0.70272	-0.352801	1.252741	738192.	1.33954	1.67810
62					0.92573	-0.077177	1.511609	98667.	1.56471	2.36522
63					0.77262	-0.257965	1.185754	766822.	1.52273	1.80558
64					1.21403	0.193942	1.518761	130995.	2.04094	3.09970
65					0.99323	-0.006792	1.782528	79485.	2.04072	3.63764
72					0.21844	-1.521263	1.288191	152338.	0.43189	0.55636
93					0.61425	-0.487354	1.363911	227952.	1.36097	1.85624
94					1.11243	0.106544	1.638132	54460.	1.73138	2.83623
96					2.75229	1.012433	1.070160	97059.	10.18187	10.89623
					1.82199	0.599928	1.360283	1261703.	4.99150	6.78986

I	J	K	L	M	N	FAKTOR F	LOG F	S-WERTE	N-WERTE	P-WERTE	SPP-WERTF
	2					0.909228	-0.095100	1.231086	5920226.	2.81684	3.46777
	3					0.68094	-0.384422	1.827032	1784871.	1.68037	3.07009
						1.68007	0.518835	1.122615	1168392.	6.03889	6.77934
01						1.16644	0.154130	1.364999	1108457.	3.65509	4.98917
02						3.06471	1.119952	1.600656	342039.	8.49497	13.59752
03						2.74110	1.009359	2.035530	37804.	5.54736	11.29181
04						0.93731	-0.064746	1.218653	1772757.	2.93077	3.57159
05						0.60796	-0.497808	1.374595	1337800.	1.69170	2.32549
06						0.69684	-0.361202	1.409671	2169039.	1.53030	2.15722
07						0.57606	-0.549975	2.028332	253717.	1.01077	2.05017
08						0.50430	-0.684582	1.861185	404139.	1.09438	2.03684
09											
10						0.45321	-0.791398	2.125382	372656.	0.73632	1.56495

# ITERATIVE SOLUTION OF EQ. (8') OF THE "DESCRIPTION" (APP 1)

Appendix 2B

$\Delta = 1.000$      $\beta = 0.0$      $C = 0.0$      $D = 0.0$      $E = 0.0$      $F = 1.000$   
 $N = 8966800.$      $P = 2.89642$      $Q = 2.89642$      $R = 1.000061$

STUFE 0    S = 1.089530

0	0.24773	0.31909	0.96677	0.26837	0.12945	0.91049	2.88682	2.06416	0.51300	0.18590
1	0.91603	4.69370	0.31014	0.15614	0.89537	0.36547	3.19380	1.39424	0.87958	5.87692
2	3.87528	1.43274	4.51325	3.73742	2.54897	0.52864	0.46248	0.54022	0.52573	0.70464
3	0.70457	0.14911	0.46988	0.59776	3.51533					
4	1.72333	0.97252	0.58015							
5	2.08495	1.26193	2.93292	1.91525	1.01186	0.58407	0.52834	0.34897	0.37784	0.25422

STUFE 1    S = 0.999999

0	0.16719	0.18107	0.85562	0.28010	0.13930	1.04270	2.57094	2.42023	0.30387	0.12454
1	0.54058	3.16707	0.37092	0.23454	0.89947	0.38076	2.14791	1.42913	0.60704	2.97137
2	3.99325	1.68628	4.06824	3.85344	1.47689	0.49156	0.56223	0.60010	0.66448	0.78254
3	0.57544	0.16798	0.43314	0.81294	2.73944					
4	1.74006	1.00121	0.49192							
5	2.05763	1.15586	2.62650	1.82698	1.03336	0.57463	0.67736	0.38132	0.35859	0.26891

CTICE 10

S = 0.999999

U	0.16505	0.17817	0.05144	0.27575	0.10991	1.04966	2.77068	2.56827	0.29453	0.12319
	0.53074	3.19966	0.34714	0.19046	0.91781	0.38489	2.20162	1.46075	0.61963	2.95746
	3.85490	1.65635	3.97172	3.78064	1.49779	0.48322	0.57870	0.59161	0.66180	0.76009
	0.60224	0.16066	0.43725	0.74405	2.60518					
V	1.76382	0.99794	0.48743							
W	2.04733	1.14659	2.61293	1.80207	1.03119	0.57723	0.69433	0.38283	0.35000	0.27052

I	J	K	L	M	N	FAKTOR F	LOG F	S-WERTE	N-WERTE	P-WERTE	S*P-WERTIF
02						0.16505	-1.801480	1.000016	204259.	0.71752	0.71753
04						0.17817	-1.724989	1.000017	107557.	0.92421	0.92422
11						0.85144	-0.160822	1.000015	1481350.	2.80019	2.80023
12						0.27575	-1.288278	1.000013	429943.	0.77731	0.77732
14						0.10991	-2.208115	1.000016	315714.	0.37494	0.37495
15						1.04946	0.048471	1.000014	842067.	2.63715	2.63719
16						2.77048	1.019092	1.000016	141758.	8.36144	8.36158
18						2.56827	0.943231	1.000016	324732.	5.97867	5.97877
21						0.29653	-1.215598	1.000016	42552.	1.48587	1.48590
22						0.12319	-2.094033	1.000013	29681.	0.53846	0.53847
23						0.53074	-0.633482	1.000013	20759.	2.65321	2.65324
24						3.19945	1.163045	1.000012	40951.	13.59493	13.59510
26						0.34714	-1.058040	1.000014	46679.	0.89830	0.89832
27						0.19046	-1.658327	1.000014	579006.	0.45224	0.45225
28						0.91741	-0.085770	1.000015	479516.	2.59336	2.59340
31						0.38489	-0.954707	1.000013	262705.	1.05854	1.05855
33						2.20162	0.789194	1.000016	114557.	9.25059	9.25074
34						1.46075	0.378948	1.000015	100276.	4.03831	4.03837
36						0.61963	-0.478628	1.000015	50980.	2.54764	2.54768
38						2.95746	1.084399	1.000017	78076.	17.02205	17.02234
42						3.85489	1.349342	1.000017	82478.	11.22446	11.22465
45						1.65636	0.504623	1.000016	481095.	4.14983	4.14990
46						3.97172	1.379199	1.000017	83965.	13.07227	13.07250
48						3.78068	1.329903	1.000017	138700.	10.82514	10.82533
51						1.49779	0.403990	1.000014	68853.	7.38290	7.38300
52						0.48322	-0.727278	1.000016	72621.	1.53115	1.53118
53						0.57870	-0.546975	1.000015	738192.	1.33954	1.33956
62						0.59741	-0.514823	1.000018	98667.	1.56471	1.56473
63						0.66190	-0.412791	1.000015	766822.	1.52273	1.52275
64						0.76099	-0.273141	1.000016	130995.	2.04094	2.04098
65						0.60224	-0.507105	1.000017	79485.	2.04072	2.04076
72						0.16046	-1.928467	1.000017	152338.	0.43189	0.43190
91						0.43725	-0.827259	1.000014	227952.	1.36097	1.36099
94						0.74405	-0.295648	1.000015	54460.	1.73138	1.73140
96						2.60518	0.957502	1.000016	97059.	10.18187	10.18204
						1.76392	0.567484	0.999998	1261703.	4.99150	4.99140

1	2	3	K	L	M	N	FAKTOR F	LOG F	S-WERTE	N-WERTE	P-WERT F	S*O-WERT F
							0.99704	-0.002062	1.000000	5920226.	2.81684	2.81684
							0.48743	-0.718609	1.000024	1784871.	1.68037	1.68041
							2.04723	0.716534	1.000014	1168392.	6.03889	6.03897
							1.14659	0.136789	1.000008	1108457.	3.65508	3.65516
							2.61293	0.960474	1.000015	342039.	8.49497	8.49516
							1.80267	0.588935	1.000010	37804.	5.54734	5.54742
							1.03119	0.030711	1.000011	1772757.	2.93077	2.93080
							0.57723	-0.549513	1.000020	1337800.	1.69176	1.69174
							0.69433	-0.364802	1.000019	2169039.	1.53030	1.53033
							0.38283	-0.960175	1.000011	253717.	1.01077	1.01076
							0.35900	-1.024429	1.000008	404139.	1.09438	1.09438
							0.27052	-1.307426	1.000011	372656.	0.73632	0.73632

From appendices 2A and 2B the following can be computed

•  $m = \text{number of cells} = 35 \times 3 \times 10 = 1,050$  Degrees of Freedom (important part) =  $35 + 3 + 10 - 3 + 1 = 46$

•  $\min \chi^2 = \hat{Q}_A$  of reaction 3 of main paper = 2 obs claims cost  $\times (5-1)$ , taken from 2A, =  
 $= 2 \times \text{NP} \times (5-1) = 2 \times 8,966,800 \times 2.89462 \times 0.331231 = 17,205,210$

•  $\hat{\sigma}^2$  of reaction 3 =  $\hat{Q}_A / m = 1,624.0$   $\hat{\sigma}^2_{\text{unbiased}} = \hat{Q}_A / (m-46) = 1,698.4$   $\hat{\sigma} = 41.2$

•  $2 \log L = -m (\log \hat{Q}_A + \frac{1}{36} \sum \log v_i + \frac{1}{3} \sum \log v_j + \frac{1}{10} \sum \log w_k) = -1,050 \log \hat{Q}_A + 521.1$

• E.g. the hypothesis of no premium differentiation has  $2 \log L_1 = -1,050 \hat{Q}_A'$  where  
 $\hat{Q}_A' \geq \hat{Q}_A$  i.e.  $-1,050 \log \hat{Q}_A' \leq -1,050 \hat{Q}_A$  so

$2 \log L - 2 \log L_1 \geq 521.1$  to be compared with  $\chi^2$  with  $46-1 = 45$  degrees of Freedom, a highly significant deviation.

Mottagare	Datum	Ev. klassificering	Sida
	82-08-10		1 (6)
Arbets ärende	Utfärdare-ref.	Björn Ajne	



## Home-owner's comprehensive as an illustration of multiplicative rate making.

### 1. Short description of home-owner's comprehensive

Home-owner's comprehensive in my company consists of two parts, viz. insurance for the building and a combined householder's insurance. The latter usually covers private property within the house (carpets, furniture, TV-sets etc) against fire, water damage and burglary. It also includes cover for personal liability (as a private person, not as a house-owner) and some other things, depending on which one of three alternatives the policyholder has chosen.

In the following we will only consider the insurance for the building. It covers fire, storm, damage to windows, water damage and machinery breakdown, damage to the house in connection with burglary, and liability as a house-owner (e.g. snow from the roof causing personal damage). The two dominating risks are fire and water damage, as seen from the following table. Storm may now and then, every tenth year or so, pop up and show noteworthy figures.

Table 1. Fire and water damage claims as a percentage of total claims cost. Building insurance within home-owner's comprehensive.

Year of incurrence	73	74	75	76	77	78	79	80
Fire, %	25	31	29	29	23	28	25	25
Water damage, %	52	58	57	57	54	58	64	62
Fire + water, %	77	89	86	86	77	86	89	89

### 2. Tarif structure of building insurance

In 1979, realizing the increasing impact of water damage claims as a consequence of the increased standard in the households, we revised the tarif structure. Thus the premium was split into two parts and a new premium argument (the number of "water units", see below) was introduced.

$$P = P_1 + P_2$$

$P_1$  covers water damage and liability

$P_2$  covers remaining risks



Mottagare	Datum 82-08-10 Utförare ref. Björn Ajne	Ev. klassificering	Sida 2
Arbets ärende			

Both premiums are loaded for expenses.  $P_1$  is split into a fixed and a variable part

$$P_1 = F_1 + V_1$$

$F_1$  covers the liability risk premium and fixed expenses.

$V_1$  covers water damage and variable expenses. It is of the form

$$V_1 = B_1 10^{0.01 p_1}$$

where  $p_1$  is the total number of points of type one in our points system, see appendix 1. An increase of  $p_1$  by 30 points thus means a doubling of  $V_1$ .

We have eight premium arguments, cf appendix 1, viz.

1. Byggnadsyta (area covered by the building, length times width) in  $m^2$ . The corresponding number of points of type 1,  $p_{11}$ , is proportional to the logarithm of the area. This means that  $V_1$  is proportional to the area itself, i.e. we take out a premium per square metre of building area. This is thus our measure of exposure.
2. Hustyp, type of house. Corresponding points  $p_{12}$  (and  $p_{22}$  for  $P_2$ , see below) are given in a separate table not shown here.
3. Material (in outer walls), stone or wood, and
4. Byggnadsår, the year when the building was finished (eight classes). These two arguments are given combined points,  $p_{134}$  and  $p_{234}$ , shown in separate tables.
5. Antal våtenheter, number of water units. You have to count the total number of units connected to the water supply system of the house such as sinks, dishing machines, wash basins, washing machines, WC's, baths, separate shower baths and - if indoors - swimming pool (two units). Points,  $p_{51}$  and  $p_{52}$ , as functions of the number of water units are in separate tables.



Mottagare	Datum	Ev. klassificering	Sida
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Arbets ärenda	Utfördare ref. Björn Ajne		

6. Uppvärmningssätt, method for warming up the house (circulating water, electrical radiators, other, none - the form is used also for summer houses), and
7. Komm vatten, if water supply from a central water plant of the district or not. Points,  $p_{167}$  and  $p_{267}$ , in separate tables.
8. Belägenhet, the geographical location of the house (eight choices for permanent residence). Points,  $p_{18}$  and  $p_{28}$  in separate tables.

Thus

$$P_1 = P_{11} + P_{12} + P_{134} + P_{15} + P_{167} + P_{18}$$

so that the variable premium  $V_1$  is a product with one factor for each premium argument - arguments 3 and 4 and also 6 and 7 being combined, though (multiplicative tariff model).

The premium  $P_2$  has no fixed part (this is customary for fire dominated premiums) and so is of the form

$$P_2 = B_2 10^{0.01 p_2}$$

where  $p_2$  is the sum of points of type two,  $p_{2x}$ .

All premium arguments, with their values, are reprinted on the policy. The policy holder can thus check that the premium is founded on correct information.

### 3. Statistical analysis of the tariff structure.

The introduction of a new tariff structure in 1979 was preceded by statistical analyses, with some guessing involved as to the appearance in our portfolio of the new premium argument water unit.

Analyses were again carried out in 1980 and 1981. We will use part of the latter as an illustration of multiplicative rate making. I will mainly refer to the paper "Description of the multiplicative ratemaking model" which is included as appendix 1 in the material previously sent out.



Mottagare	Datum	Ev. klassificering	Sida
	82-08-10		4
	Utförare ref.		
	Björn Ajne		
Arbets ärende			

Appendix 2 shows a multiplicative graduation of observed water damage risk premiums. These are the base for the variable premium  $V_1$ .

Claims are censored at 50 KSEK, i.e. for each claim only the amount up to this point is taken into account.

The column N-WERTE shows exposures, marginal for each premium argument value and total, in hundreds of square metres of building area. The total exposure amounts to 424605, corresponding to some 400000 policy years (100000 policies during the four years of incurrence 1976-79).

P-WERTE are observed marginal and total risk premiums in KSEK per 100 square metres building area. Thus the total observed claims cost is

$$424605 \times 0.19759 = 83\,898 \text{ KSEK}$$

S-WERTE are the marginal and total quotients between graduated and observed claims costs referred to in the Description. As they are greater than one it is evident that the graduation has been done according to formulas (7)-(8) there. The total S, the deviation of which from one is our primary measure of goodness-of-fit, amounts to 1.552328.

FAKTOR F gives the factors for the different premium argument values. As explained in section 3 of the theoretical paper (main paper) we do not actually use these factors, but

the factors obtained from graduation according to formulas (7') and (8') in the Description. These are shown in appendix 3. The N-WERTE and P-WERTE are the same as before, but the S-WERTE are now all equal to one as they should.

The following figures may be shown

No of premium argument values						No of cells	
$m_1$	$m_2$	$m_3$	$m_4$	$m_5$	$m_6$	$m$	
8	7	6	3	2	7	14112	

$$\text{Degrees of freedom } \sum m_i - 6 + 1 = 28$$



Mottagare	Datum 82-08-10 Utfärdare, ref. Björn Ajne	Ev. klassificering	Sida 5
Arbets ärenda			

$$\hat{Q}_A = \min \chi^2 = 2 \times \text{obs claims} \times (S-1) =$$

$$= 2 \times 83898 \times 0.552328 = 92678$$

(S taken from appendix 2)

$$\hat{\sigma}^2 = \hat{Q}_A / m = 6.5673$$

$$\hat{\sigma} = 2.5627$$

In the model underlying the analysis this means that for each cell the standard deviation of the distribution of individual claims sizes equals 2.5627 times the square root of the average claims size.

Twice the log likelihood of the graduation, according to section 3 of the theoretical paper, is computed as

$$\log \hat{Q}_A = \text{constant} + \log (S-1) = C - 0.593613$$

and adding, for each premium argument, the arithmetic mean of the logarithms of its factors,

which gives, in addition -0.053594

finally multiplication by  $-m = -14112$  should be carried out which gives twice the likelihood (apart from general additive constants) as  $-14112 (C - 0.647207)$ .

#### 4. Comparisons between tariff structures

In the analysis described above, material and age of building were combined while the remaining premium arguments were supposed to have independent multiplicative factors in the risk premium.

Several analyses were carried out, in which different groups of arguments were combined. As an illustration the loglikelihood for one additional such analysis is given below together with the loglikelihood above and the loglikelihood for the structure with no premium differentiation at all between cells, i.e. all factors equal to one.



Mottagare	Datum 82-08-10	Ev. klassificering	Sida 6
	Utfärdare ref. Björn Ajne		

Arbets ärende

	(i)	(ii)	(iii)
	No premium differentiation	Material and Age combined	Material and Age and No. of water units combined
d.f.	1	28	70
S	1.789470	1.552328	1.505716
log (S-1)	-0.236393	-0.593613	-0.681780
Sum of means of logfactors	0	-0.053594	0.013516
2xLoglikelihood /-14.112	C-0.236393	C-0.647207	C-0.668264

To test (i) against (ii) the difference between twice the loglikelihoods is taken and compared to chi-square with  $28-1 = 27$  d.f.

$$14112 (0.647207 - 0.236393) = 5797$$

which is highly significant.

The corresponding difference for testing (ii) against (iii), with 42 d.f., is

$$14112 (0.668264 - 0.647207) = 297.2$$

which is highly significant (above the 99.9 percentile), too, though to a lesser extent.

The reduction of (S-1), compared to no premium differentiation, is 30 % for structure (ii) and 36 % for structure (iii).

##### 5. What happened to the tariff?

In spite of the foregoing result, Water units were not combined with Material and Age in tariff 82. Reasons of complexity and statistical instability could be invoked against a structure with many parameters.

Material and Age are combined, however, and so are the arguments for Warming up method and Central water plant.

In appendix 4, the tariff factors for no. of water units are compared to those in the statistical analysis of appendix 3. As seen, the tariff does not incorporate the full effect of the observed differentiation. Confidence intervals may be pretty wide, though.

## APPENDIX 1

## Kunduppgifter

Fyll inte i rastrode fält = Skandias noteringar

<input checked="" type="checkbox"/> Villaförsäkring	<input type="checkbox"/> Fritidshusförsäkring	<input type="checkbox"/> Separat lösöreförsäkring
Begynnelsedatum (år-mån-dag)		
Namn		
Björn Ajne		
Utleveringsadress		
Kritvägen 3		
Postnummer och ortnamn		
141 34 Huddinge		
Fastighetsbeteckning och kommun		
Flyttblocket 21		
Huddinge		

### Personlig lösegendom

Omfattning				Försäkr. bel. kr
<input type="checkbox"/> Stor	<input type="checkbox"/> Liten	<input type="checkbox"/> Mini	<input type="checkbox"/> Fritidshus	
Om. Förh. vid skad. risk		Typ	Medförsäkrads namn	
		kr		

\* 1000 hrs forking over to the (Kashmiri) ...

**Huvudbyggnad** Se anvisningar på blankettens baksida

1 Byggnadsyta (utvändiga mått i markplan) längd x bredd = 130 m<sup>2</sup>

2 Hustyp

1 En våning utan källare och utan inredd vind 	2 En våning utan källare men med inredd vind 	3 En våning med källare men utan inredd vind 	4 En våning med källare och inredd vind 
5 Två våningar utan källare och utan inredd vind 	6 Två våningar med källare men utan inredd vind 	7 Två våningar utan källare men med inredd vind 	8 Två våningar med källare och inredd vind 
9 Tre eller flera våningar 			

3 Material i yttervägg

☒ Sten ☐ Trä

4 Byggnadsår 1965

5 Antal våneheter  
 Var god fyll i blankettens baksida = 12 stycken

6 Uppvärmningssätt

☒ Cirkulerande varmvatten ☐ Elektriska radiatorer ☐ Annan uppvärmning ☐ Ingen uppvärmning

7 Komm vatten

☒ Ja ☐ Nej

8 Belägenhet

☐ 1 ☐ 2 ☐ 3 ☒ 4 ☐ 5 ☐ 6 ☐ 7 ☐ 8 ☐ 9

Omf Förhöjd stöterisk 1,000 kr Typ Förstärksbelopp kkr\* Brand/Allt framtid kkr\*

### Övriga byggnader

Nr	Benämning	Byggnads yta	Vinterbonat	Om	Kranor	Typ	Typ
		m <sup>2</sup>	<input type="checkbox"/> Ja <input type="checkbox"/> Nej				kk <sup>a</sup>
		m <sup>2</sup>	<input type="checkbox"/> Ja <input type="checkbox"/> Nej				kk <sup>a</sup>
		m <sup>2</sup>	<input type="checkbox"/> Ja <input type="checkbox"/> Nej				kk <sup>a</sup>

### Övriga uppgifter

Husbocksförsäkring		Ersätter husbocksförsäkring i (bolagets namn)	
<input type="checkbox"/> Ja	<input type="checkbox"/> Nej		
Skandirakonto		Bank- giro	Past- giro
<input type="checkbox"/> önskas	<input type="checkbox"/> finns	<input type="checkbox"/>	<input type="checkbox"/>
Har Ni tidigare haft hem-, villa- eller fridshusförsäkring i annat bolag?		<input type="checkbox"/> Ja	<input type="checkbox"/> Nej
Tidigare försäkringsbolag			
Blev försäkringen uppsagd eller endast förnyad mot tilläggspremie?		<input type="checkbox"/> Ja	<input type="checkbox"/> Nej
		Har Ni haft mer än en skada under de senaste 12 månaderna?	<input type="checkbox"/> Ja <input type="checkbox"/> Nej

Personnummer (10 siffror)		Codenr	
c	35	03	04 04 99 02
Nyteckning		Omskrivning	
Förlösd, försäkring		At ZK risk	
Förlösd, bestånd		Ja	
Specialaviserings		Kontroll	
OS	ICA	02	Skandia
Annan förfallodag			
Ersatt försäkring nr			
Kommunkod	Försäkringsberäkn. kr	Distrib. bevakning	
Påslag/Rabatt löseendom		Premie löseendom	
%	Typ		
Points of type		Självriskfaktor	
1	2	=	→ Löseendom
Poäng 1	Poäng 2	Premie Huvudbyggnad	
53	53	Premie 1 + 515 ← P <sub>1</sub>	
		Premie 2 + 184 ← P <sub>2</sub>	
		Avdrag all framtid -	
4	15	= 699	
Fri = 0	Fri = 0	Självriskfaktor 0,90 ← Rabate factor deduct.	
20	0	Huvudbyggnad + 629	
60	10	= 629 -	
19	8	Påslag/Rabatt Huvudbyggnad	
16	16	% Typ	
Summa 1	Summa 2		
172	102		
Påslag/Rabatt Övriga byggnader		P <sub>2</sub>	
%	Typ	Övrig byggnad +	
%	Typ	Övrig byggnad +	
%	Typ	Övrig byggnad +	
		Husbock +	
Total premie kronor			
Noteringar			
Handläggare			

(incc ccvv)

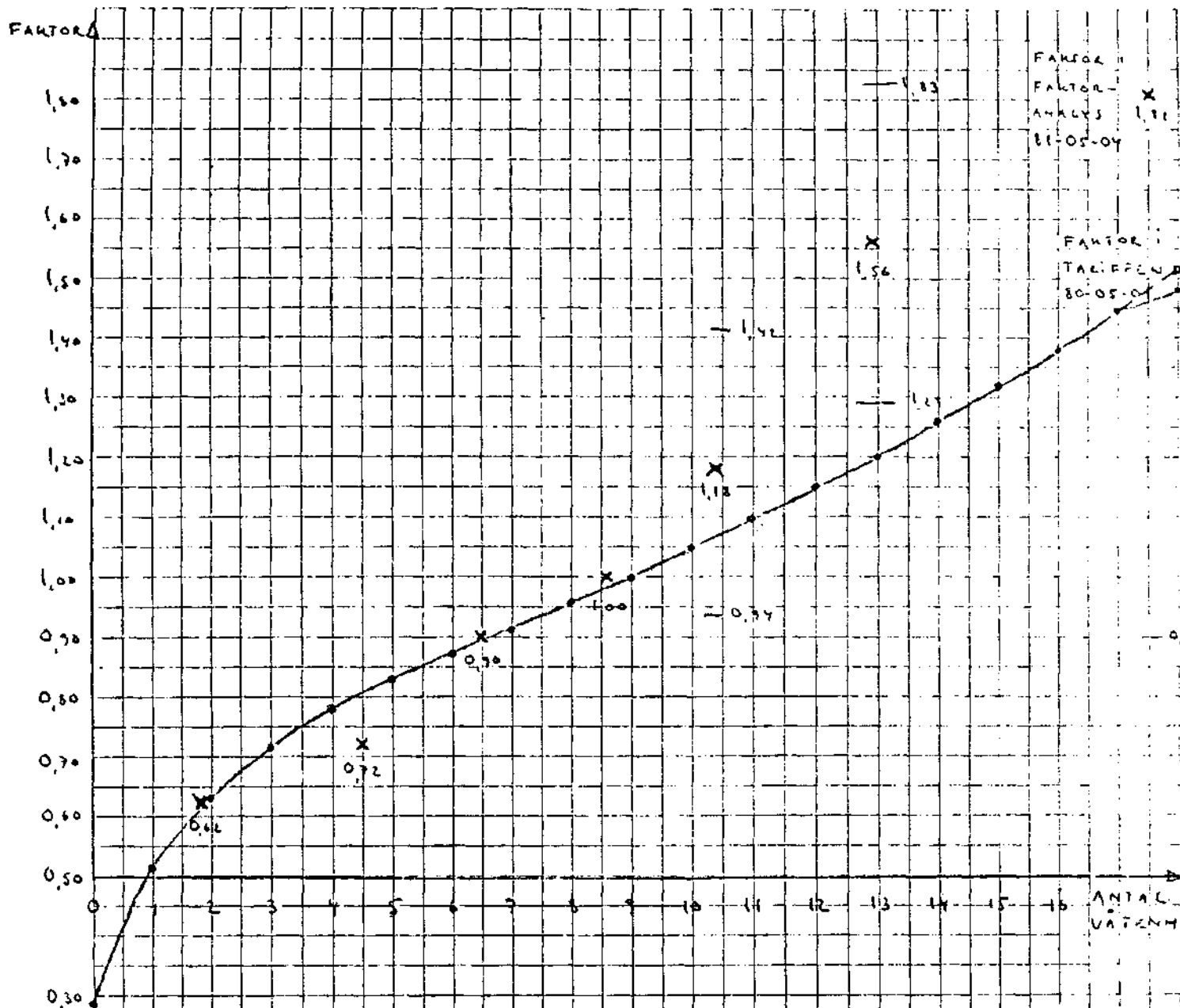
# APPENDIX 2

I	J	K	L	M	N	FACTOR F	Q-WERTE	S-WERTE	N-WERTE	P-WERTE	MEDELOUSUM
502	Material x Age of building (4 classes)					1.69832	1.193927	1.952937	24459.	0.15047	0.46272E+01
509						1.59483	1.151731	1.404454	76139.	0.19575	0.18633E+01
519						1.89364	1.245986	1.366957	69040.	0.21606	0.20319E+01
599						1.09249	1.213164	1.660935	44389.	0.19482	0.25988E+01
T02	building (4 classes)					1.41731	1.202765	2.372066	33089.	0.12235	0.41618E+01
T09						1.51137	1.185424	1.514817	69060.	0.19379	0.24082E+01
T19						1.73239	1.229287	1.609576	98510.	0.22339	0.39280E+01
T99						1.65467	1.363299	1.501180	71041.	0.22417	0.25683E+01
3	0-3	4-5	6-7	8-9	10-11	0.89644	1.651949	2.906545	23289.	0.11704	0.48428E+01
						0.76953	1.245355	1.847799	52040.	0.14327	0.21058E+01
						0.83295	1.208090	1.484864	71546.	0.14564	0.16685E+01
						0.92130	1.122092	1.444588	102676.	0.18687	0.14255E+01
9	12-15	16-	1	2	3	0.94487	1.123857	1.354022	114556.	0.20191	0.13481E+01
						1.39555	1.084204	1.462454	53796.	0.28936	0.40494E+01
						3.07201	1.349604	2.727624	6858.	0.37481	0.41672E+02
						0.85289	1.347764	1.708292	95105.	0.14712	0.18828E+01
11	4	5	6	7	8	1.01270	1.325772	1.529068	74443.	0.19234	0.21686E+01
						0.88915	1.163685	1.514752	100803.	0.16923	0.26634E+01
						1.11356	1.184691	1.521857	52644.	0.22713	0.31628E+01
						1.11559	1.273140	1.505052	58654.	0.23842	0.32231E+01
15	5	6	7	8	9	1.24453	1.121955	1.392984	43072.	0.29259	0.42136E+01
						0.94537	1.153989	1.411240	265123.	0.21660	0.21716E+01
						0.99177	1.224332	1.739982	149732.	0.16611	0.26093E+01
						1.82524	1.491286	3.662278	9846.	0.16377	0.18240E+02
90	6	7	8	9	10	1.41580	1.367163	2.714273	50755.	0.15749	0.79558E+01
						0.91310	1.160614	1.423486	373919.	0.20303	0.19851E+01
						1.10609	1.181500	1.321895	21878.	0.18735	0.37996E+01
						0.67035	1.137278	1.423865	142150.	0.14539	0.10226E+01
7	3	4	5	6	7	1.04210	1.154585	1.438247	79795.	0.22287	0.25616E+01
						0.87125	1.383226	1.565212	99161.	0.17446	0.16848E+01
						1.34631	1.182567	1.527461	50655.	0.27978	0.46387E+01
						1.81403	1.211332	1.741374	25780.	0.31402	0.82528E+01
1	2	3	4	5	6	1.79803	1.520453	2.141401	15324.	0.22214	0.70934E+01
						1.22031	1.552328	424695.	0.19750	0.2699538780+01	

# APPENDIX 3

≈1 (incre. ccv8v)

I	J	K	L	M	N	FAKTOR F	Q-WERTE	S-WERTE	N-WERTE	P-WERTE	MEDELQUSUM
S02						0.74672	0.954017	1.000128	24469.	0.15047	0.36820E+01
S09						0.95290	0.922842	1.000088	76139.	0.19575	0.14930E+01
S19						1.09329	0.906093	0.999964	69090.	0.21606	0.14777E+01
S99						1.07074	0.880023	0.999998	44389.	0.19482	0.18852E+01
T02						0.56915	0.932285	1.000095	33089.	0.12235	0.32259E+01
T09						0.92555	0.913214	1.000136	68060.	0.19370	0.18552E+01
T19						1.07561	0.915604	0.999964	38510.	0.22339	0.29257E+01
T99						1.12532	0.794533	0.999956	71041.	0.22417	0.14968E+01
	3					0.58868	0.929913	0.999982	23280.	0.11704	0.27261E+01
	5					0.68263	0.888369	0.999976	52040.	0.14327	0.15022E+01
	7					0.85392	0.908794	0.999993	71546.	0.18564	0.12551E+01
	9					0.94798	0.857472	1.000000	102676.	0.18687	0.10893E+01
	11					1.11682	0.872954	0.999985	114556.	0.20191	0.10425E+01
	15					1.47671	0.862109	0.999975	53796.	0.28936	0.32199E+01
	99					1.71513	0.970659	1.000015	6858.	0.37481	0.29977E+02
		1				0.82743	0.891835	1.000073	95105.	0.14712	0.12458E+01
		2				1.11554	0.911252	0.999984	74443.	0.19234	0.14894E+01
		3				0.83307	0.952972	0.999936	100803.	0.16923	0.21811E+01
		4				1.11883	0.864045	0.999926	52664.	0.22713	0.22971E+01
		5				1.16326	0.906013	0.999901	58654.	0.23842	0.22847E+01
		6				1.28979	0.848468	0.999919	43072.	0.29259	0.31865E+01
			1			1.04939	0.866995	0.999970	265123.	0.21660	0.16233E+01
			2			0.92397	0.925918	0.999965	149732.	0.16611	0.19669E+01
			3			0.96430	0.967681	0.999956	9846.	0.16377	0.11836E+02
				E		0.88790	0.957169	0.999893	50755.	0.15749	0.55700E+01
				V		1.01715	0.873615	0.999906	373919.	0.20303	0.14942E+01
					1	0.91666	0.931929	0.999996	21878.	0.18735	0.29968E+01
					2	0.75742	0.831916	0.999968	142169.	0.14539	0.74799E+00
					3	1.15210	0.913150	0.999966	79785.	0.22287	0.20191E+01
					4	0.81404	0.938330	1.000072	88161.	0.17446	0.11429E+01
					5	1.38000	0.874949	0.999984	50655.	0.27978	0.34379E+01
					6	1.63500	0.895071	1.000018	26780.	0.31402	0.61047E+01
					7	1.33013	0.980355	1.000004	15324.	0.22214	0.45737E+01
							0.900029	1.000254	424605.	0.19759	0.1982054110+01



Relative sizes of factors for no. of water units in tariff 80 (V1)

Deviation in tariff 81 (only for the highest no. exhibited in this figure, viz. 18)

X Observed relative sizes in the analysis described in the text (placed over the portfolio points of gravity for the seven intervals studied)